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§ 1065.275 N2O measurement devices.

(a) General component requirements.

We recommend that you use an analyzer that meets the specifications in Table 10f 40 CFR 1065.205. Note that your system must meet the linearity verification in 40 CFR 1065.307.

(b) Instrument types.

You may use any of the following analyzers to measure N2O:

(1) Nondispersive infra-red (NDIR) analyzer.

You may use an NDIR analyzer that has compensation algorithms that are functions of other gaseous measurements and the engine's known or assumed fuel properties. The target value for any compensation algorithm is 0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias.

(2) Fourier transform infra-red (FTIR) analyzer.

You may use an FTIR analyzer that has compensation algorithms that are functions of other gaseous measurements and the engine's known or assumed fuel properties. The target value for any compensation algorithm is 0.0% (that is, no bias high and no bias low), regardless of the

uncompensated signal's bias. Use EPA Test Method 320 "Measurement of Vapor Phase Organic and Inorganic Emissions by Extractive Fourier Transform Infrared (FTIR) Spectroscopy" for spectral interpretation (see 40 CFR part 63 appendix A).

(3) Photoacoustic analyzer.

You may use a photoacoustic analyzer that has

compensation algorithms that are functions of other gaseous measurements. The target value for any compensation algorithm is 0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use an optical wheel configuration that gives analytical priority to measurement of the least stable components in the sample. Select a sample integration time of at least 5 seconds. Take into account sample chamber and sample line volumes when determining flush times for your instrument.

(4) Gas chromatograph (GC) analyzer.

You may use a gas chromatograph with Electron Capture Detector (ECD) to measure N₂O concentrations of diluted exhaust for batch sampling. You may use a packed or porous layer open tubular (PLOT) column phase of suitable polarity and length to achieve adequate resolution of the N₂O peak for analysis. Examples of acceptable columns are a PLOT column consisting of bonded polystyrenedivinylbenzene or a Porapack Q packed column. Take the column temperature profile and carrier gas selection into

consideration when setting up your method to achieve adequate N₂O peak resolution.

(c) Interference validation.

Perform interference validation for NDIR, FTIR, and Photoacoustic analyzers using the procedures of § 86.168– 12 as follows:

(1) Certain interference gases can positively interfere with these analyzers by causing a response similar to N₂O as follows:

(i) The interference gases for NDIR analyzers are CO, CO₂, H₂O, CH₄ and SO₂. Note that interference species, with the exception of H₂O, are dependent on the N₂O infrared absorption band chosen by the instrument manufacturer and should be determined independently for each analyzer.
(ii) Use good engineering judgment to determine interference gases for FTIR. Note that interference species, with the exception of H₂O, are dependent on the N₂O

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§ 1065.275 N2O measurement devices.

(a) *General component requirements*. We recommend that you use an analyzer that meets the specifications in Table 1 of §1065.205. Note that your system must meet the linearity verification in §1065.307.

(b) *Instrument types*. You may use any of the following analyzers to measure N₂O:

(1) Nondispersive infra-red (NDIR) analyzer. You may use an NDIR analyzer that has compensation algorithms that are functions of other gaseous measurements and the engine's known or assumed fuel properties. The target value for any compensation algorithm is 0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. (2) Fourier transform infra-red (FTIR) analyzer. You may use an FTIR analyzer that has compensation algorithms that are functions of other gaseous measurements and the engine's known or assumed fuel properties. The target value for any compensation algorithm is 0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use appropriate analytical procedures for interpretation of infrared spectra. For example, EPA Test Method 320 is considered a valid method for spectral interpretation (see

http://www.epa.gov/ttn/emc/methods/method320.html).

(3) *Photoacoustic analyzer*. You may use a photoacoustic analyzer that has compensation algorithms that are functions of other gaseous measurements. The target value for any compensation algorithm is 0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use an optical wheel configuration that gives analytical priority to measurement of the least stable components in the sample. Select a sample integration time of at least 5 seconds. Take into account sample chamber and sample line volumes when determining flush times for your instrument. (4) *Gas chromatograph analyzer*. You may use a gas chromatograph with an electron-capture detector (GC–ECD) to measure N₂O concentrations of diluted exhaust for batch sampling.

(i) You may use a packed or porous layer open tubular (PLOT) column phase of suitable polarity and length to achieve adequate resolution of the N_2O peak for analysis. Examples of acceptable columns are a PLOT column consisting of bonded polystyrene-divinylbenzene or a Porapack Q packed column. Take the column temperature profile and carrier gas selection into consideration when setting up your method to achieve adequate N_2O peak resolution.

(ii) Use good engineering judgment to zero your instrument and correct for drift. You do not need to follow the specific procedures in §1065.530 and §1065.550(b) that would otherwise apply. For example, you may perform a span gas measurement before and after sample analysis without zeroing. Use the average area counts of the pre-span and post-span measurements to generate a response factor (area counts/span gas concentration), which you then multiply by the area counts from your sample to generate the sample concentration.

(c) *Interference validation*. Perform interference validation for NDIR, FTIR, and photoacoustic analyzers using the procedures of <u>\$1065.375</u>. Interference validation is not required for GC–ECD. Certain interference gases can positively interfere with NDIR, FTIR, and photoacoustic analyzers by causing a response similar to N₂O. When running the interference verification for these analyzers, use interference gases as follows:

 infrared absorption band chosen by the instrument manufacturer and should be determined independently for each analyzer. (iii) The interference gases for photoacoustic analyzers are CO, CO₂, and H₂O. (2) Analyzers must have combined interference that is within (0.0 +/- 1.0) mol/mol. We strongly recommend a lower interference that is within (0.0 +/- 0.5) mol/. 9. A new § 86.168–12 is added to subpart B to read as follows: 	 (1) The interference gases for NDIR analyzers are CO, CO₂, H₂O, CH₄and SO₂. Note that interference species, with the exception of H₂O, are dependent on the N₂O infrared absorption band chosen by the instrument manufacturer and should be determined dently for each analyzer. (2) Use good engineering judgment to determine interference gases for FTIR. Note that interference species, with the exception of H₂O, are dependent on the N₂O infrared absorption band chosen by the instrument manufacturer and should be determined independently for each analyzer. (3) The interference gases for photoacoustic analyzers are CO, CO₂, and H₂O.
 § 86.168–12 Interference verification for N-O analyzers. (a) Scope and frequency. See 40 CFR 1065.275 to determine whether you need to verify the amount of interference after initial analyzer installation and after major maintenance. (b) Measurement principles. Interference gasses can positively interfere with certain analyzers by causing a response similar to N₂O. If the analyzer uses compensation algorithms that utilize measurements of other gases to meet this interference verification, simultaneously conduct these other measurements to test the compensation algorithms during the analyzer interference verification. (c) System requirements. See 40 CFR 1065.275 for system requirements related to allowable interference levels. (d) Procedure. Perform the interference verification as follows: (1) Start, operate, zero, and span the N₂O FTIR analyzer as you would before an emission test. If the sample is passed through a dryer during emission testing, you may run this verification test with the dryer if it meets the requirements of 40 CFR 1065.342. Operate the dryer at the same conditions as you will for an emission test. You may also run this verification test without the sample dryer. (2) Create a humidified test gas by bubbling a multi component span gas that incorporates the target interference species and meets the specifications in 40 CFR 1065.750 through distilled water in a sealed vessel. If the sample is not passed through a dryer during emission testing, control the vessel temperature to generate an H₂O level at least as high as the level determined in 40 CFR 1065.145(e)(2) for that dryer. Use interference span gas concentrations that are at least as high as the maximum expected during testing. (4) If the sample is not passed through a dryer during this verification test, measure the water mole fraction, xHD, of the humidified interference test gas into the sample system. You may introduce it d	§ 1065.375 Interference verification for N ₂ O analyzers. (a) <i>Scope and frequency</i> . See §1065.275 to determine whether you need to verify the amount of interference after initial analyzer installation and after major maintenance. (b) <i>Measurement principles</i> . Interference gasses can positively interfere with certain analyzers by causing a response similar to N ₂ O. If the analyzer uses compensation algorithms that utilize measurements of other gases to meet this interference verification, simultaneously conduct these other measurements to test the compensation algorithms during the analyzer interference verification. (c) <i>System requirements</i> . Analyzers must have combined interference that is within $(0.0 \pm 1.0) \mu$ mol/mol. We strongly recommend a lower interference that is within $(0.0 \pm 0.5) \mu$ mol/mol. (d) <i>Procedure</i> . Perform the interference verification as follows: (1) Start, operate, zero, and span the N ₂ O analyzer as you would before an emission test. If the sample is passed through a dryer during emission testing, you may run this verification test with the dryer if it meets the requirements of \$1065.342. Operate the dryer at the same conditions as you will for an emission test. You may also run this verification test with the dryer at the sample is not passed through a dryer during emission testing. Control the vessel temperature to generate an H ₂ O level at least as high as the maximum expected during emission testing, control the vessel temperature to generate an H ₂ O level at least as high as the evel determined in \$1065.145(e)(2) for that dryer. Use interference span gas concentrations that are at least as high as the level determined in \$1065.145(e)(2) for that dryer. Use interference test gas as close as possible to the inlet of the analyzer. For example, measure dewpoint, <i>T</i> dew, and absolute pressure, <i>p</i> total, to calculate <i>x</i> H _{2O} . Verify that the water content meets the requirement in paragraph (d)(2) of this section. If the sample is passed through a dryer during testing, dryer du
vessel pressure and temperature. Use good engineering judgment to estimate the water content. For example, you	may use previous direct measurements of water content to verify the vessel's level of saturation.

may use previous direct measurements of water content to	(5) If a sample dryer is not used in this verification test, use
verify the vessel's level of saturation.	good engineering judgment to prevent condensation in the
(5) If a sample dryer is not used in this verification test, use	transfer lines, fittings, or valves from the point where x_{H20} is
good engineering judgment to prevent condensation in the	measured to the analyzer. We recommend that you design
transfer lines, fittings, or valves from the point where <i>x</i> H20 is measured to the analyzer. We recommend that you design	your system so that the wall temperatures in the transfer lines, fittings, and valves from the point where x_{H2O} is
your system so that the wall temperatures in the transfer lines, fittings, and valves from the point where <i>x</i> _{H20} is	measured to the analyzer are at least 5 °C above the local sample gas dewpoint.
measured to the analyzer are at least 5 °C above the local	(6) Allow time for the analyzer response to stabilize.
sample gas dewpoint.	Stabilization time may include time to purge the transfer line
(6) Allow time for the analyzer response to stabilize.	and to account for analyzer response.
Stabilization time may include time to purge the transfer line	(7) While the analyzer measures the sample's concentration,
and to account for analyzer response.	record its output for 30 seconds. Calculate the arithmetic
(7) While the analyzer measures the sample's concentration,	mean of this data.
record its output for 30 seconds. Calculate the arithmetic	(8) The analyzer meets the interference verification if the
mean of this data.	result of paragraph (d)(7) of this section meets the tolerance
(8) The analyzer meets the interference verification if the	in paragraph (c) of this section.
result of paragraph $(d)(7)$ of this section meets the tolerance	(9) You may also run interference procedures separately for
in 40 CFR 1065.275.	individual interference gases. If the interference gas levels
(9) You may also run interference procedures separately for	used are higher than the maximum levels expected during
individual interference gases. If the interference gas levels	testing, you may scale down each observed interference
used are higher than the maximum levels expected during	value by multiplying the observed interference by the ratio
testing, you may scale down each observed interference	of the maximum expected concentration value to the actual
value by multiplying the observed interference by the ratio	value used during this procedure. You may run separate
of the maximum expected concentration value to the actual	interference concentrations of H ₂ O (down to 0.025 mol/mol
value used during this procedure. You may run separate	H_2O content) that are lower than the maximum levels
interference concentrations of H2O (down to 0.025 mol/mol	expected during testing, but you must scale up the observed
H2O content) that are lower than the maximum levels	H ₂ O interference by multiplying the observed interference
expected during testing, but you must scale up the observed	by the ratio of the maximum expected H ₂ O concentration
H2O interference by multiplying the observed interference	value to the actual value used during this procedure. The
by the ratio of the maximum expected H2O concentration	sum of the scaled interference values must meet the
value to the actual value used during this procedure. The	tolerance specified in paragraph (c) of this section.
sum of the scaled interference values must meet the	
tolerance specified in 40 CFR 1065.275.	
§ 86.167–12 №O measurement devices.	-
(a) <i>General component requirements</i> . We recommend that you use an analyzer	
that meets the specifications in Table 1	
of 40 CFR 1065.205. Note that your	
system must meet the linearity	
verification in 40 CFR 1065.307.	
(b) <i>Instrument types</i> . You may use any	
of the following analyzers to measure	
N2O:	
(1) Nondispersive infra-red (NDIR)	
analyzer. You may use an NDIR	
analyzer that has compensation	
algorithms that are functions of other	
gaseous measurements and the engine's	
known or assumed fuel properties. The	
target value for any compensation	
algorithm is 0.0% (that is, no bias high	
and no bias low), regardless of the	
uncompensated signal's bias.	
(2) Fourier transform infra-red (FTIR)	
analyzer. You may use an FTIR analyzer	
that has compensation algorithms that	
are functions of other gaseous	
measurements and the engine's known	
or assumed fuel properties. The target	
value for any compensation algorithm is	
0.0% (that is, no bias high and no bias	
0.0% (that is, no bias high and no bias low), regardless of the uncompensated	
0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use EPA Test Method 320	
0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use EPA Test Method 320 "Measurement of Vapor Phase Organic	
0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use EPA Test Method 320 "Measurement of Vapor Phase Organic and Inorganic Emissions by Extractive	
0.0% (that is, no bias high and no bias low), regardless of the uncompensated signal's bias. Use EPA Test Method 320 "Measurement of Vapor Phase Organic	

intermentation (and 10 CED (2)	[]
interpretation (see 40 CFR part 63	
appendix A).	
(3) <i>Photoacoustic analyzer</i> . You may	
use a photoacoustic analyzer that has	
compensation algorithms that are	
functions of other gaseous	
measurements. The target value for any	
compensation algorithm is 0.0% (that is,	
no bias high and no bias low), regardless	
of the uncompensated signal's bias. Use an optical wheel	
configuration that § 86.111–94 Exhaust gas analytical	896 111 04 Exhaust gas analytical surface
system.	<pre>\$86.111-94 Exhaust gas analytical system. * * * * *</pre>
****	(b) Major component description. The exhaust gas analytical
(b) Major component description. The	system, Figure B94–7, consists of a flame ionization detector
exhaust gas analytical system, Figure	(FID) (heated, 235 °±15 °F (113 °±8 °C) for methanol-fueled
B94–7, consists of a flame ionization	vehicles) for the determination of THC, a methane analyzer
detector (FID) (heated, 235 ° } 15 °F	(consisting of a gas chromatograph combined with a FID) for
$(113^{\circ} \ 8^{\circ}\text{C})$ for methanol-fueled	the determination of CH4, non-dispersive infrared analyzers
vehicles) for the determination of THC,	(NDIR) for the determination of CO and CO2, a
a methane analyzer (consisting of a gas	chemiluminescence analyzer (CL) for the determination of
chromatograph combined with a FID)	NOX, and an analyzer meeting the requirements specified in
for the determination of CH4, nondispersive	40 CFR 1065.275 for the determination of N2O (required for
infrared analyzers (NDIR) for	2015 and later model year vehicles). A heated flame
the determination of CO and CO ₂ , a	ionization detector (HFID) is used for the continuous
chemiluminescence analyzer (CL) for	determination of THC from petroleum-fueled diesel-cycle
the determination of NOx, and an	vehicles (may also be used with methanol-fueled diesel-cycle
analyzer meeting the requirements	vehicles), Figure B94–5 (or B94–6). The analytical system
specified in § 86.167–12 for the	for methanol consists of a gas chromatograph (GC) equipped
determination of N2O for 2012 and later	with a flame ionization detector. The analysis for
model year vehicles. A heated flame	formaldehyde is performed using high-pressure liquid
ionization detector (HFID) is used for	chromatography (HPLC) of 2,4-dinitrophenylhydrazine
the continuous determination of THC	(DNPH) derivatives using ultraviolet (UV) detection. The
from petroleum-fueled diesel-cycle	exhaust gas analytical system shall conform to the following
vehicles (may also be used with	requirements: 1267
methanol-fueled diesel-cycle vehicles),	* * * *
Figure B94–5 (or B94–6). The analytical	
system for methanol consists of a gas	6. Section 86.113-04 is amended by revising the entry for
chromatograph (GC) equipped with a	RVP in the table in paragraph $(a)(1)$ to read as follows:
flame ionization detector. The analysis	it in the table in paragraph (a)(1) to read as follows.
for formaldehyde is performed using	
high-pressure liquid chromatography	
(HPLC) of 2,4-dinitrophenylhydrazine	
(DNPH) derivatives using ultraviolet	
(UV) detection. The exhaust gas	
analytical system shall conform to the following requirements:	
ioliowing requirements:	
4. Section 86.127–00 is amended as	
follows:	
a. By revising the introductory text.	
b. By revising paragraph (a)	
introductory text.	
c. By revising paragraph (a)(1),	
d. By revising paragraph (b).	
e. By revising paragraph (c).	
f. By revising paragraphs (d) and (e).	
1. Dy tovising paragraphs (u) and (c).	

§ 1065.205 Performance specifications for measurement instruments.

Your test system as a whole must meet all the applicable calibrations, verifications, and test-validation criteria specified in subparts D and F of this part or subpart J of this part for using PEMS and for performing field testing. We recommend that your instruments meet the specifications in Table 1 of this section for all ranges you use for testing. We also recommend that you keep any documentation you receive from instrument manufacturers showing that your instruments meet the specifications in Table 1 of this section.

Table 1 of §10	065.205-Recomme	nded performance spec	cifications for measu	rement instrum	ents	
Measurement Instrument	Measured quantity symbol	Complete System Rise time (\underline{t}_{10-90}) and Fall time (\underline{t}_{90-10}) ^a	Recording update frequency	Accuracy ^b	Repeatability ^b	Noise ^b
Engine speed transducer	fn	1 s	1 Hz means	2.0 % of pt. or 0.5 % of max.	1.0 % of pt. or 0.25 % of max.	0.05 % of max
Engine torque transducer	Т	l s	1 Hz means	2.0 % of pt. or 1.0 % of max.	1.0 % of pt. or 0.5 % of max	0.05 % of max.
Electrical work (active-power meter)	W	l s	l Hz means	2.0 % of pt. or 0.5 % of max.	1.0 % of pt. or 0.25 % of max.	0.05 % of max
General pressure transducer (not a part of another instrument)	р	5 s	1 Hz	2.0 % of pt. or 1.0 % of max.	1.0 % of pt. or 0.50 % of max.	0.1 % of max
Atmospheric pressure meter used for PM- stabilization and balance environments	$p_{\rm atmos}$	50 s	5 times per hour	50 Pa	25 Pa	5 Pa
General purpose atmospheric pressure meter	Patmos	50 s	5 times per hour	250 Pa	100Pa	50 Pa
Temperature sensor for PM-stabilization and balance environments	Т	50 s	0.1 Hz	0.25 K	0.1 K	0.1 K
Other temperature sensor (not a part of another instrument)	T	10 s	0.5 Hz	0.4 % of pt. K or 0.2 % of max. K	0.2 % of pt. K or 0.1 % of max. K	0.1 % of max
Dewpoint sensor for PM-stabilization and balance environments	$T_{ m dew}$	50 s	0.1 Hz	0.25 K	0.1 K	0.02 K
Other dewpoint sensor	$T_{\rm dew}$	50 s	0.1 Hz	1 K	0.5 K	0.1 K
Fucl flow meter (Fuel totalizer)	m	5 s (N/A)	1 Hz (N/A)	2.0 % of pt. or 1.5 % of max.	1.0 % of pt. or 0.75 % of max.	0.5 % of max.
Total diluted exhaust meter (CVS) (With heat exchanger before meter)	'n	l s (5 s)	l Hz means (1 Hz)	2.0 % of pt. or 1.5 % of max.	1.0 % of pt. or 0.75 % of max.	1.0 % of max.
Dilution air, inlet air, exhaust, and sample flow meters	'n	1 s	1 Hz means of 5 Hz samples	2.5 % of pt. or 1.5 % of max.	1.25 % of pt. or 0.75 % of max.	1.0 % of max.
Continuous gas analyzer	x	5 s	1 Hz	2.0 % of pt. or 2.0 % of meas.	1.0 % of pt. or 1.0 % of meas.	1.0 % of max.
Batch gas analyzer	x	N/A	N/A	2.0 % of pt. or 2.0 % of meas.	1.0 % of pt. or 1.0 % of meas.	1.0 % of max.
Gravimetric PM balance	m _{PM}	N/A	N/A	See §1065.790	0.5 µg	N/A
Inertial PM balance	m _{PM}	5 s	l Hz	2.0 % of pt. or 2.0 % of meas.	1.0 % of pt. or 1.0 % of meas.	0.2 % of max.

^a The performance specifications identified in the table apply separately for rise time and fall time. ^b Accuracy, repeatability, and noise are all determined with the same collected data, as described in §1065.305, and based on absolute values. "pt." refers to the overall flow-weighted mean value expected at the standard; "max." refers to the peak value expected at the standard over any test interval, not the maximum of the instrument's range; "meas" refers to the actual flow-weighted mean measured over any test interval.